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# Parametric Study on Axial Force in Steel and CFRP cables for a Cable-stayed bridge

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Abstract— Man's achievement in field of Structural Engineering is evident from world's tallest structures to largest bridge spans etc. In the recent years cable stayed bridges have received more attention than any other bridges mainly, in the United States, Japan and Europe as well as in third-world counties due to their ability to cover large spans. Cable-stayed bridge can cross almost 1000m. A study is carried out to find the axial force on different types of cables on a cable stayed bridge. The different types of cables used are steel and CFRP. The study is carried out on Akkar Bridge in Sikkim which is India's first cable stayed bridge. Live loads are taken according to IRC 6:2000, IRC Class 70R vehicle load was considered. A Dynamic analysis in the form of Non-Linear Time-history is also carried out using Cape, Kobe and CFRP cables are represented.

Keywords—Time history analysis, axial force, cable stayed bridge, CFRP, Steel

#### I. INTRODUCTION

The past two or three decades has outfitted the wide application of Cable-stayed bridges in different parts of the world. Varied long span application of cable-stayed bridges has been established just recently, with the initiation of highstrength steel and FRP materials, evolution of advanced welding techniques, different deck shapes, and the advancement in structural analysis. The assortment of shapes and forms of cable-stayed bridges mesmerize even the most demanding designers, architects as well as the common people. Engineers are developing them both innovating and challenging. Cable-stayed bridges are considered as one of the most fetching recent development in the stream of bridge engineering. Increased application of these bridges among bridge engineers are often accredited to its appealing aesthetics, full and economical utilization of structural elements, augmented stiffness over long span suspension bridges, efficient and quicker mode of construction and comparatively tiny size of their substructure.

Cable-stayed bridges are best suited for spans shorter than suspension bridges and longer than cantilever bridges. The span length lies in range where a cantilever bridge would be really heavy and suspension bridge will be not practical because using large amount of cables for a shorter span bridge will be uneconomical. [7] proposed a system, this fully automatic vehicle is equipped by micro controller, motor Reshma Prasad Department of Civil Engineering FISAT Kochi, India reshma.prasad@gmail.com

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driving mechanism and battery. The power stored in the battery is used to drive the DC motor that causes the movement to AGV. The speed of rotation of DC motor i.e., velocity of AGV is controlled by the microprocessor controller.

The main objective of this study is to find out the axial force developed in the steel cables of Akkar Bridge and compare them by replacing the cables using CFRP strands. The study aims to find out which of the two materials performs better under dead load, moving load and earthquake loads.

#### II. BRIDGE DATA

For the study Akkar bridge is considered. The Akkar Bridge at Jorethang, South Sikkim, over Rangit River is India's first cable-stayed concrete bridge (Fig.1). It was completed in 1988 and was constructed by Gammon India.

• H Shape

PYLON

- The second second
- Total height: 54.6m
- Height below deck: 20.7m
- Height above deck: 33.9m
- Top section : 1.61x1.61m
- Bottom section: 2.5x2.5m

#### DECK

- Total width: 10m
- Width of Roadway: 2 lane 7.5m
- Depth: 0.180m
- Span: 154m



Fig.1. Akkar Bridge



International Journal of Advanced Research Trends in Engineering and Technology (IJARTET) Vol. 4, Special Issue 15, March 2017

# CABLES

- Cable Section: 37 H.T E450 wires (Area = 1423.9  $mm^2$ )
- Number of Cables : 34
- Prestressing force: 2280kN

## GIRDERS

- Longitudinal girder: 0.6x0.8m concrete • frame element
- Cross girders: 0.45x0.8m concrete frame element at 3m intervals

#### CONCRETE

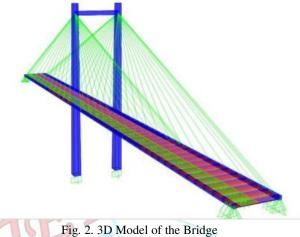
- Grade: M45
- Weight/unit volume: 25 kg/m<sup>3</sup>
- Modulus of Elasticity: 33541 MPa
- Poissons ratio: 0.2

## A. Modeling of Cables

The cable element is modeled as a linear frame. The modeling of cables is a difficult issue because of nonlinearities arises from the cable sag. The stiffness thus changes when load is applied. A prestessing force of 2280kN was applied to all the cables in order to ensure a small deformation of the deck when the self-weight is applied.

## B. Properties of CFRP

- Weight/unit volume: 15.68 kg/m<sup>3</sup>
- Modulus of Elasticity: 160000 MPa
- Poissons ratio: 0.3



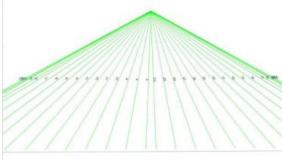
# STEEL(Cables)

- Grade: E450 (Fe570)
- Weight/unit volume : 76.9729 kg/m<sup>3</sup>
- Modulus of Elasticity: 199000 MPa
- Poissons ratio: 0.3

# ECFRP X ACFRP = Esteel X Asteel

C. Equivalent Area of CFRP Cables

 $1.6 \times 10^8 \text{ x A}_{\text{CFRP}} = 1.99 \times 10^8 \times 1423.9 \times 10^7$  $A_{CFRP} = 1.77 \times 10^{-3} m^2$ 



#### Fig. 3 .Cables

# III. MODELING

CSi Bridge is a powerful and versatile tool for analysis and design of structures based on static and dynamic finite element analysis. Non-linear analysis can also be performed in CSi. Bridge. The analytical capabilities are just powerful representing the latest research in numerical techniques and solution algorithms. The program is structured to support wide variety of the latest national and international codes for both concrete and steel.



International Journal of Advanced Research Trends in Engineering and Technology (IJARTET) Vol. 4, Special Issue 15, March 2017

IV. RESULTS

Steel Dead (kN)	CFRP Dead (kN)	Steel vehicle (kN)	CFRP vehicle (kN)	
0.127	0.00009684	60.144	60.134	
0.126	0	60.702	60.693	
0.125	0	61.268	61.258	
3.138	1.815	61.227	61.218	
43.788	41.742	58.353	58.345	
115.512	112.258	52.592	52.586	
301.657	295.646	106.172	106.134	
465.487	457.759	180.23	180.18	
559.187	551.17	223.499	223.453	
589.135	581.926	238.744	238.707	
568.802	562.488	239.902	239.869	
517.914	512.444	236.5	236.468	
450.253	445.847	232.655	232.625	
384.997	381.604	229.052	229.023	
338.512	335.571	225.335	22 <mark>5.307</mark>	
307.566	304.276	21 <mark>4.</mark> 266	214.24	
285.038	281.393	18 <mark>8.557</mark>	188.539	
285.038	<b>281.393</b>	188. <mark>557</mark>	188.539	
307.567	304.277	214.266	214.24	
338.512	335.571	225.335	225.307	
384.998	381.605	229.052	229.023	
450.254	445.847	232.655	232.625	
517.914	512.444	236.5	236.4 <mark>68</mark>	
568.802	562.488	239.902	239.869	
589.135	581.927	238.744	238.707	
559.187	551.17	223.499	223.453	
465.487	457.759	180.23	180.18	
301.657	295.646	106.172	106.134	
115.512	112.258	52.592	52.586	
43.788	41.742	58.353	58.345	
3.138	1.815	61.227	61.218	
0.125	0	61.268	61.258	
0.126	0	60.702	60.693	
0.127	0.00009679	60.144	60.134	

Steel	CFRP	
(kN)	(kN)	
35.223	33.679	
35.86	34.309	
36.516	34.959	
41.184	39.774	
83.786	80.951	
162.029	156.418	
354.723	346.162	
519.451	509.057	
606.49	595.818	
622.662	614.644	
625.605	617.498	
588.047	580.405	
512.3	505.925	
459.095	451.055	
408.529	401.263	
345.828	339.999	
304.624	301.602	
310.201	305.876	
363.248	357.554	
413.996	407.313	
461.011	453.658	
508.765	500.936	
575.286	566.525	
646.11	635.833	
674.4	662.832	
635.536	626.189	
556.508	546.697	
383.72	375.787	
180.132	175.55	
100.115	96.881	
64.179	61.574	
60.49	57.973	
59.53	57.029	
58.596	56.109	

Table.2. Axial Force in Cables- Cape EQ

Table.1. Axial Force in Cables- Dead and Moving load Case (Moving Load – IRC Class 70R through one lane)

CFRP (kN)

25.722

25.917

26.113

30.27

65.109

128.277

307.671

471.203

569.919

593.115

574.166

516.867

475.542

422.768

373.834

330.106

279.583

279.296

332.913 384.688

432.199

482.901

523.311

606.482

579.298

470.922

302.011

123.238

59.446 25.733

21.834

21.703

21.572

572.19



International Journal of Advanced Research Trends in Engineering and Technology (IJARTET) Vol. 4, Special Issue 15, March 2017

(kN) = (kN) = (kN) $30.314 = 27.364$ $30.759 = 27.796$ $31.216 = 28.239$ $34.614 = 32.994$ $32.75$ $70.092 = 70.74$ $32.75$ $70.092 = 70.74$ $32.75$ $70.092 = 70.74$ $32.75$ $70.092 = 70.74$ $32.75$ $70.092 = 70.74$ $32.75$ $32.68.619$ $579.804 = 570.539$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $579.27$ $607.584 = 598.9$ $314.28$ $488.00$ $282.96$ $335.44$ $283.60$ $282.96$ $335.44$ $283.60$ $282.96$ $335.44$ $283.60$ $282.96$ $335.44$ $283.60$ $288.00$ $580.43$ $615.63$ $580.433$ $615.63$ $588.4493 = 575.315$ $484.472 = 475.577$ $321.894 = 315.984$ $479.80$ $308.72$ $143.403 = 140.006$ $72.87 = 70.622$ $33.737 = 31.941$			Steel	CFRP		Steel
30.314       27.364         30.759       27.796         31.216       28.239         34.614       32.994         70.092       70.74         136.997       137.011         316.811       309.461         484.439       476.082         579.804       570.539         607.584       598.9         576.179       568.619         516.436       510.632         466.569       461.227         413.113       408.693         314.526       310.169         284.197       279.909         292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						28.108
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		30.759				28.312
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		31.216				28.518
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						32.756
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						68.213
316.811       309.461         484.439       476.082         579.804       570.539         607.584       598.9         576.179       568.619         516.436       510.632         466.569       461.227         413.113       408.693         314.526       310.169         284.197       279.909         292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						132.098
484.439       476.082         579.804       570.539         607.584       598.9         576.179       568.619         516.436       510.632         466.569       461.227         413.113       408.693         359.901       356.281         314.526       310.169         282.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						314.285
$\begin{array}{c} 579.804 & 570.539 \\ \hline 607.584 & 598.9 \\ \hline 576.179 & 568.619 \\ \hline 516.436 & 510.632 \\ \hline 466.569 & 461.227 \\ \hline 413.113 & 408.693 \\ \hline 359.901 & 356.281 \\ \hline 314.526 & 310.169 \\ \hline 284.197 & 279.909 \\ \hline 292.003 & 287.369 \\ \hline 325.87 & 320.782 \\ \hline 363.758 & 359.111 \\ \hline 404.21 & 399.267 \\ \hline 450.17 & 443.713 \\ \hline 518.899 & 515.412 \\ \hline 576.929 & 572.802 \\ \hline 607.139 & 598.548 \\ \hline 584.493 & 575.315 \\ \hline 484.472 & 475.757 \\ \hline 321.894 & 315.984 \\ \hline 143.403 & 140.006 \\ \hline 72.87 & 70.622 \\ \hline 33.737 & 31.941 \\ \end{array}$						480.04
607.584       598.9         576.179       568.619         516.436       510.632         466.569       461.227         413.113       408.693         359.901       356.281         314.526       310.169         284.197       279.909         292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						579.275
576.179       568.619         516.436       510.632         466.569       461.227         413.113       408.693         359.901       356.281         314.526       310.169         284.197       279.909         292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						601.745
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						582.641
466.569       461.227         413.113       408.693         359.901       356.281         314.526       310.169         284.197       279.909         292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						524.161
413.113       408.693         359.901       356.281         314.526       310.169         284.197       279.909         292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941				6 6		482.149
359.901       356.281         314.526       310.169         284.197       279.909         292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941		413.113	100 23	1		428.051
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		359.901	356.281		a an	379.084
284.197       279.909         292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941					5 166	335.444
292.003       287.369         325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						283.63
325.87       320.782         363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						282.967
363.758       359.111         404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941		1		T		338.418
404.21       399.267         450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						390.116
450.17       443.713         518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						438.075
518.899       515.412         576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						489.738
576.929       572.802         607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						530.709
607.139       598.548         584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941				-	ACK P	580.431
584.493       575.315         484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941				710	AL	615.631
484.472       475.757         321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941						588.942
321.894       315.984         143.403       140.006         72.87       70.622         33.737       31.941				-0		479.807
72.87         70.622         127.08           33.737         31.941         62.56						308.723
72.87         70.622         62.56           33.737         31.941         28.32						127.085
33./3/ 31.941 28.32						62.562
	F					28.328
29.142 27.466 24.34						24.344
28.719 27.047	F					24.202
28 308 26 638	L	28.308	26.638			24.059

Table.3. Axial Force in Cables- El Centro EQ

Table.4. Axial Force in Cables- Kobe EQ

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#### V. CONCLUSION

The above study was conducted to compare the axial forces developed in steel and CFRP cables for a cable stayed bridge. Dead, moving and earthquake loads were considered for the same and in all the load cases CFRP cables showed less axial force values. This shows that for an equal area, CFRP cables performs better in both dead and moving load cases showing 5-10% reduction. The time-history analysis revealed a similar trend showing 3-5% reduction.

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